

In-situ resin infiltration of 3D printed porous structures



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ABSTRACT

Currently, three-dimensional (3D) printing is still a very popular manufacturing technology. However, the porous structures printed by selective laser melting (SLM) technology are still porous. Generally, the in-situ resin infiltration (CVD) method is used to fill the pores of 3D printed structures. As a result, the CVD method is still a very time-consuming process. In this paper, a new method of 3D printing porous structures is proposed. The 3D printed porous structures are filled with a conductive resin (EMIS) with a porosity of 88%–27%. The electromagnetic interference (EMI) shielding effectiveness (SE) of the porous structures is 47.8 dB at 2.7 GHz and 32.3 dB at 18 GHz. The results show that the SLM porous structures

1. Introduction

Generally, the porous structures are used in many fields, such as aerospace, automotive, and marine. The porous structures are usually made by powder metallurgy (PM) [1], foam [2], or 3D printing [3]. The porous structures are usually made by powder metallurgy (PM) [1], foam [2], or 3D printing [3]. The porous structures are usually made by powder metallurgy (PM) [1], foam [2], or 3D printing [3].

(2DG), the porous structures [5], system [6,7], systems [4], the electromagnetic interference (EMI) shielding [8] system. The porous structures are usually made by powder metallurgy (PM) [1], foam [2], or 3D printing [3]. The porous structures are usually made by powder metallurgy (PM) [1], foam [2], or 3D printing [3].

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t lyst. T i es e i t isti s (i ., e esitie i e-
 st t), t t i i fl e t fi l i est t
 (i ., l y t i ss, f ts) e f t 3DG. B si s, t
 t 3DG i i t t e e t i s f e t t l t l t
 (i ., e esity, e si s, s f lity). H e , est e f t e e s
 t l t l t s y e t i e l t e s i f f i lty
 i e sly l t i e esity, f e i st , t e i l Ni f e
 lly st e esity y e l y e t e l l f e l t
 e t t, t s s tly e t i 3DG s e s e e t e l e f e-
 s e i i e s e i f t s f e s i f i f t i e l s i 17,18].
 H e , it is e f ssity t e l e t l t l t s, i
 i s l y i l t f e e t e i e s t s t e i 3DG i t
 t l st t s s t l f e s 19].
 S l t i l s l t i (SLM), s i e t i i t i -
 f t i (AM) t e l e y, i s t i l l y s i f e t f i t i e
 e f s e l s t i t / e i s t - i s i e l (3D) t l t l t s
 i t t t s e f e l i t y i s i , f f i i y i e t i e
 f l i lity e f *in-situ* f t i i lity. T e t , e s
 s s e t SLM e e s s t t s e f T i l l e y s 20],
 s t i l s l l e y s 21], N i l l e y s 22]. C i s t e s t i l y s f e l /
 s s t t f e l - s y t s i i s t t - e f t - t -
 s i s t i l s. C e i t N i e e t s s t t,
 e i s s e s i l s s t t f e e t
 i CVD t e t l e e s t t i e l l (< 0.001 t.%)
 e t e s s s l f - l i t i e f e , i t t e t i -
 lity s i l l y i t l s 23]. W i l N i s
 i e s e l i lity (> 0.1 t.%) 17], t i f i l s t
 t e f e s e f s s i e i t i e 24]. H e , -
 s i SLM e f e i s s t i l l i t s i f y s e f i s f f i i t
 t i f e e s l t i i f e i t s i t i s i i t l
 e t i lity f l t i lity t e s e e l s l t
 (1000–1100). F i t i e e f i s e s e s f f e l s
 i SLM i s s t i l l f i y l l s 25].
 T e e e l i t i e s, f e t f i s t t i e e s
 f s i l e t t e - e t e e 3DG/ e (3DG/C) s t -
 t s i SLM s i l t e sly i e i t i e i t CVD e t e f
 . A l l - s i y e i - t y e e s e t l t s
 i i t i lly i s t i t i SLM f e i e s t t l e l t i e t e -

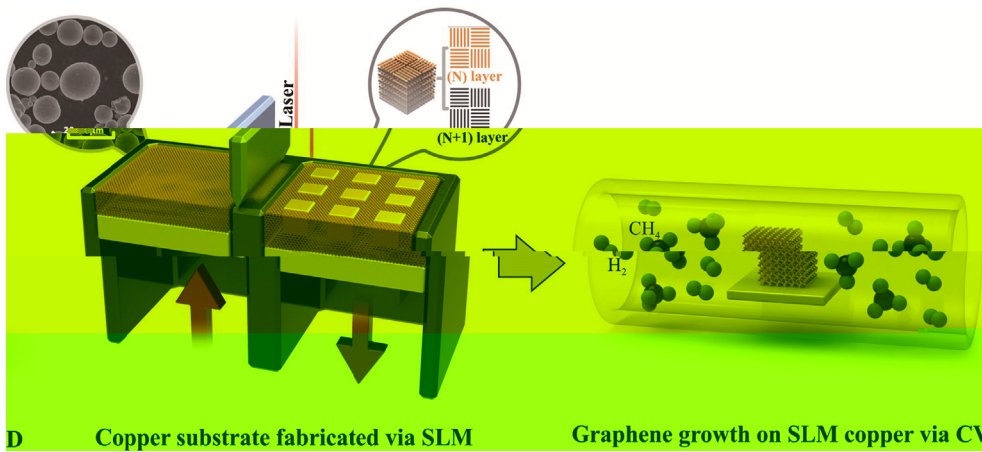


Fig. 1. Illustration of the 3DG/C composite substrate fabrication process: (a) SLM (left) *in-situ* (right) and (b) CVD (left). (For interpretation of the references to this figure legend, the reader is referred to the web version of this article.)

ASTM B193-2002 and ISO 9001:2015 standards. The tensile strength of the 3DG/C composite is 2.2–2.0 × 10³ MPa, which is higher than that of the 3DG/C substrate (5–10 × 10³ MPa). The 3DG/C composite also meets the requirements of the LFA (Laser Flash Analysis, NTS LFA457, GOM) and the SENTERRA (SENTERRA, BOMBAUDI) systems for the 3DG/C substrate. The thermal conductivity of the 3DG/C composite is 514 W/mK, which is higher than that of the 3DG/C substrate (S11–S21). The 3DG/C composite also meets the requirements of the VNA (Vector Network Analyzer, PNA-N5244A, US) system for the 2–18 GHz range. The 3DG/C composite also meets the requirements of the SEI (Scanning Electron Microscopy) and SEI (Scanning Electron Microscopy) systems (E. 2–5) for the 3DG/C composite.

3. Results and discussion

3.1. Formation of SLM copper

3.1.1. SLM manufacturing of copper under different line energy densities

The test results are shown in Fig. 2. Different laser power and scanning speed were used to fabricate the copper substrate. The results are shown in Fig. 2.

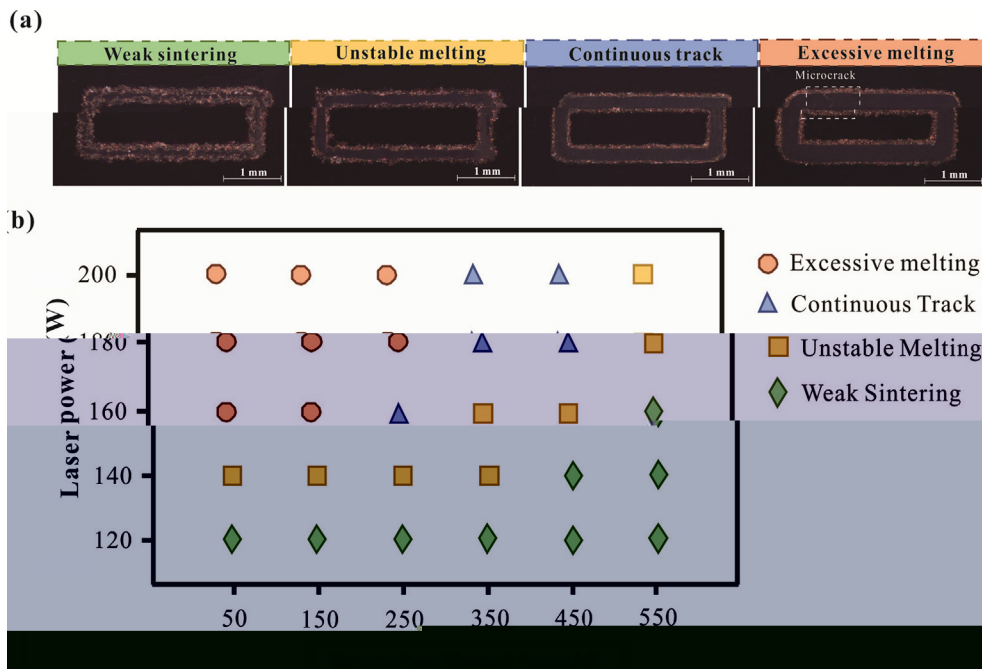


Fig. 2. (a) Typical morphology of the copper substrate under different laser power and scanning speed; (b) Typical morphology of the copper substrate under different laser power and scanning speed. (For interpretation of the references to this figure legend, the reader is referred to the web version of this article.)

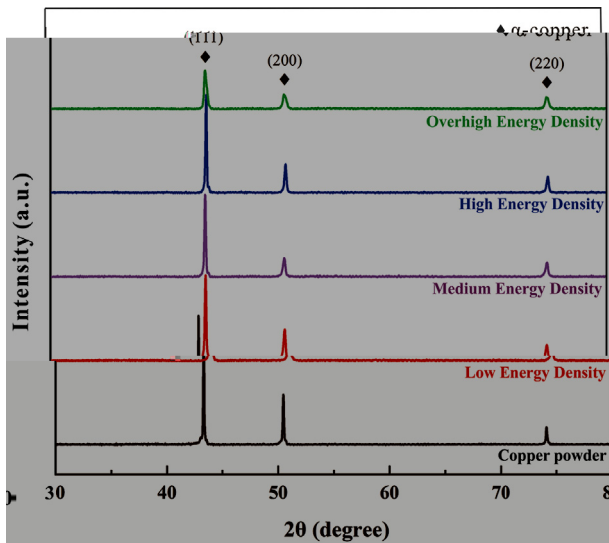


Fig. 3. RD tt s e f t s t t i e e e s - l t e s i s. (F e i t t t i e e f t f s t e e l e i t s i f i l l , t i s f t e t s i e e f t i s t i l .)

3.1.2. Formation of anisotropic microstructure under different volumetric energy density

T i s α -e e l l y t i i l l RD t t s y t (111) (200) f i t s i f f t t $2\theta = 43.32^\circ$ $2\theta = 50.45^\circ$, s t i l y (F i . 3), t (111) i t i e s i l l . T s - l t e s i s s s t s i l l RD t t s t e t s t i e t i s i i f f s i t e i t e f s i i l i f i t t i t SLM e s s . I t i e , t i f f t i e s e f SLM s l s s i f t t e i i f f t i e l s , i i t i t e f s i l l s t s s i t s - l t s l s t e t i e e l i t 29].

T e e l e y e f t e l t e l s t i e t - t i l s t i e e f t SLM e t t e l y f t i s s e f s l s i t y i y i t . T i t y s e f f t s

e s : (i) i t - l y e i s , (ii) e - l t e , (iii) s e s . A t s s i i t y e f $3000 \text{ J}/^3$ (F i . 4a), t l t e l s s i s 180μ , s i t i s i t f e t l e y e (F i . 4d). T e l t s t t s e l s t e t M e i e t i e 30] s i t i f l t t i e e t i t e l t e l . T s s t t s l t i t - l y i l s i e s i i t t e s i e s s i f i l l y l i t e i s i s i t t . W i t t i t y f t s i s s t l i t $857 \text{ J}/^3$, s e t s i t f i e s e s e t i t e l t e l s i i s s i t y t y l e s (F i . 4b). U t s e t i e s , t e t i i l y s i f i t i e t e 96.2% i t e l l i l l . H e , i t s i i t y y i t t i s t , i l e s e - l t i s s i t i e i l y s . T t i t e l t e l t s t t e t s e l t e t i t t e l t i t y e f $(398 \text{ W}^{-1} \text{ K}^{-1})$, t s i f f i t i t y s l t e l t t i l s t e e l y (F i . 4c). G s e l s e f e t i s s , i f l t e s f e t e l t e t y t M e i e t i e . B s i s , t t e s e s e t t i t t i l s y l s e l t e s s t e i s y t s l t i e s i s f e e t i e i t SLM e s s 31]. I e t s t , t l e i t y e f $128 \text{ J}/^3$, e t s e - l t e s i l l e i s e s t e l s l i t e - s l l e f i s l - l i e s , e t i f e 88.6% e f t - l t i s i t y (F i . 4d).

T e t i e e f i e t s i t SLM e s s s e t e s t t l t s (F i . 5). T y i l l i l e l l i s i l l t l i i t i e f e t - t i l s t i e , i l l y t t t e t e t y f t i f e t t t i t . T t e t i t t e t t s e l l i t f i s f e t t e t e l t e t e t e t i l l y e s t e t i e t t e t s t t , i f l i t t s t e t e l e i e s t t s 32]. T t l y i t l e t i t y e f e i s e l i s t t i t s i f s t t f l e t l i i t i e . S i l t e t e y W t l . 33], t i l l t e t s t t i t e l t l l , s l t i f e

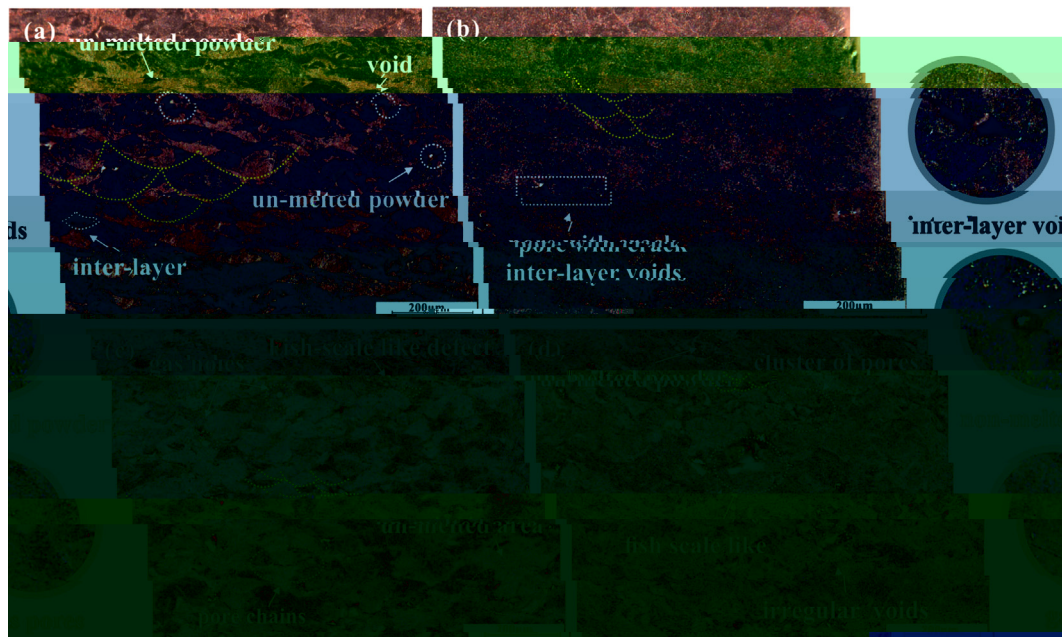


Fig. 4. O t i l l e s e f t y i l e e l e y e f s l s f i t y e s i t y i t i l i t i e : () s s i ($3000 \text{ J}/^3$), () i ($857 \text{ J}/^3$), () i ($285 \text{ J}/^3$), () e e y ($128 \text{ J}/^3$), s t i l y . (F e i t t t i e e f t f s t e e l e i t s i f i l l , t i s f t e t s i e e f t i s t i l .)

t i t e t e t s e i e i e t.

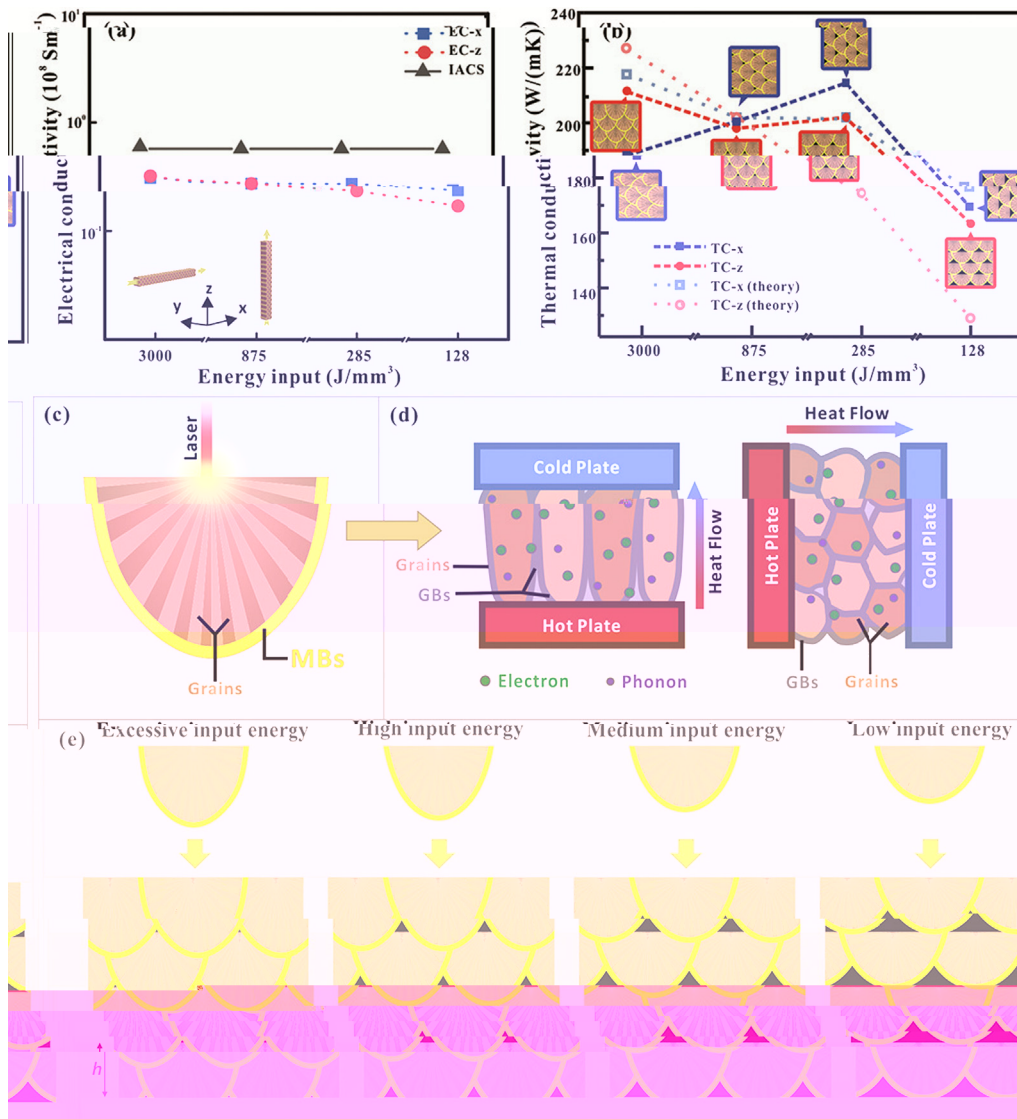


Fig. 7. (a) Electrical conductivity; (b) thermal conductivity; (c) schematic of laser irradiation; (d) schematic of heat flow; (e) schematic of grain growth under different energy inputs.

is significantly lower than that of the bulk material.

3.3. Morphology and structure of CVD 3DG/Cu porous scaffolds

The porous scaffolds with different densities were fabricated by the laser-assisted CVD method. The morphology and structure of the porous scaffolds were investigated by SEM. As shown in Fig. 8a, the porous scaffolds have a porous structure with interconnected pores. The pore size is approximately 450 μm. The porous scaffolds were fabricated by the laser-assisted CVD method. The morphology and structure of the porous scaffolds were investigated by SEM. As shown in Fig. 8a, the porous scaffolds have a porous structure with interconnected pores. The pore size is approximately 450 μm. The porous scaffolds were fabricated by the laser-assisted CVD method. The morphology and structure of the porous scaffolds were investigated by SEM. As shown in Fig. 8a, the porous scaffolds have a porous structure with interconnected pores. The pore size is approximately 450 μm.

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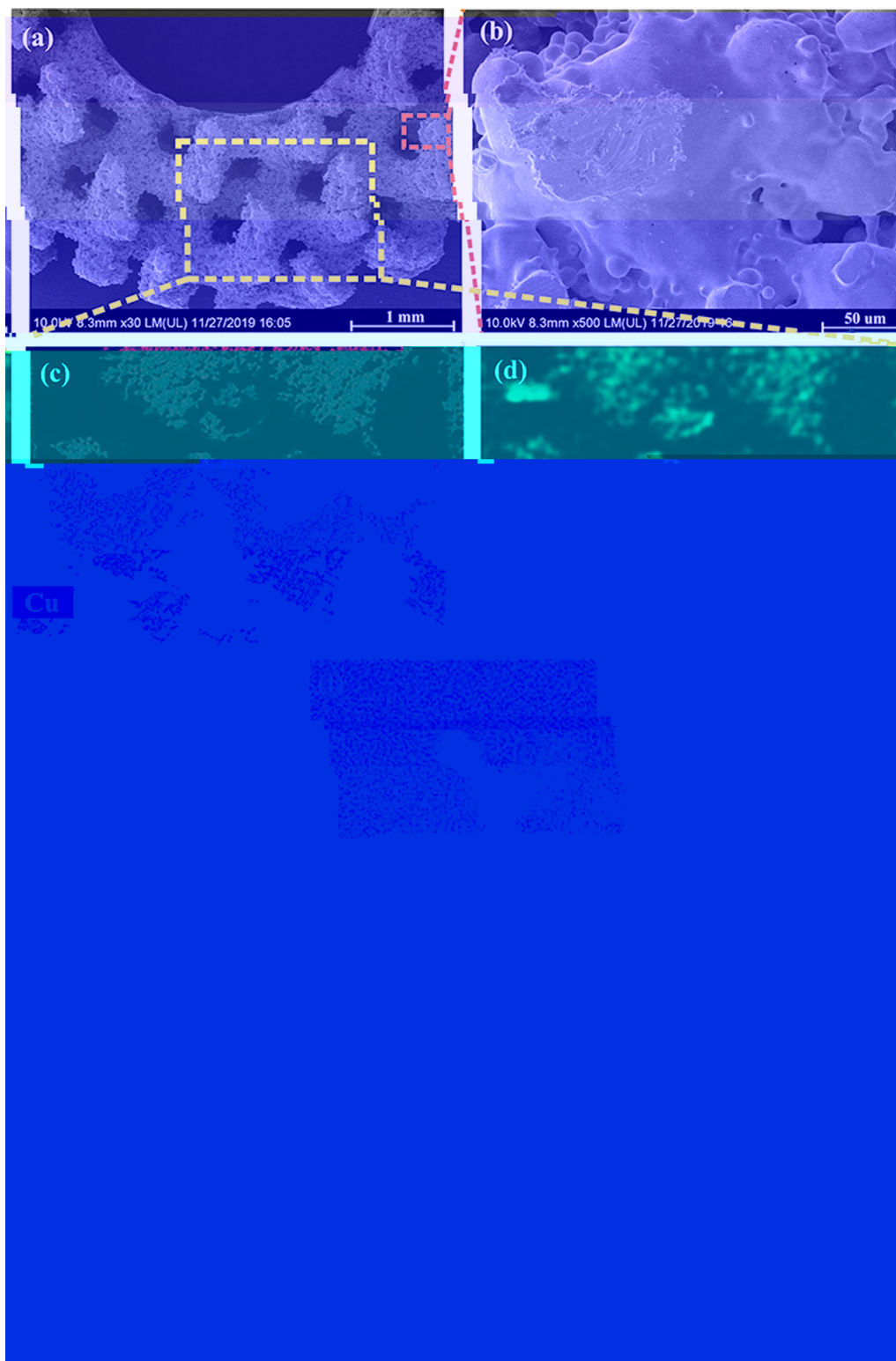


Fig. 8. (a) SEM image of 3DG/C porous scaffold; (b) High-magnification SEM image of 3DG/C porous scaffold; (c) EDS elemental map of C; (d) EDS elemental map of Cu. The scale bars are 1 mm and 50 μm, respectively.

The density of foams was measured by the Archimedes method. The ratio of I_D/I_G was in the range of 0.71 to 0.93, indicating the presence of graphite. As a result, the porous scaffold was prepared at 1000 °C for 30 s in a CH₄ atmosphere. The porous scaffold 3DG/C was synthesized.

3.4. Thermal property and EMI shielding effectiveness of 3DG/Cu porous scaffolds

The thermal stability of porous scaffolds was evaluated by TGA. The porous scaffold 3DG/C was synthesized at 26.8% Cu content, and the porous scaffold 3DG/Cu was synthesized at 14.8% Cu content.

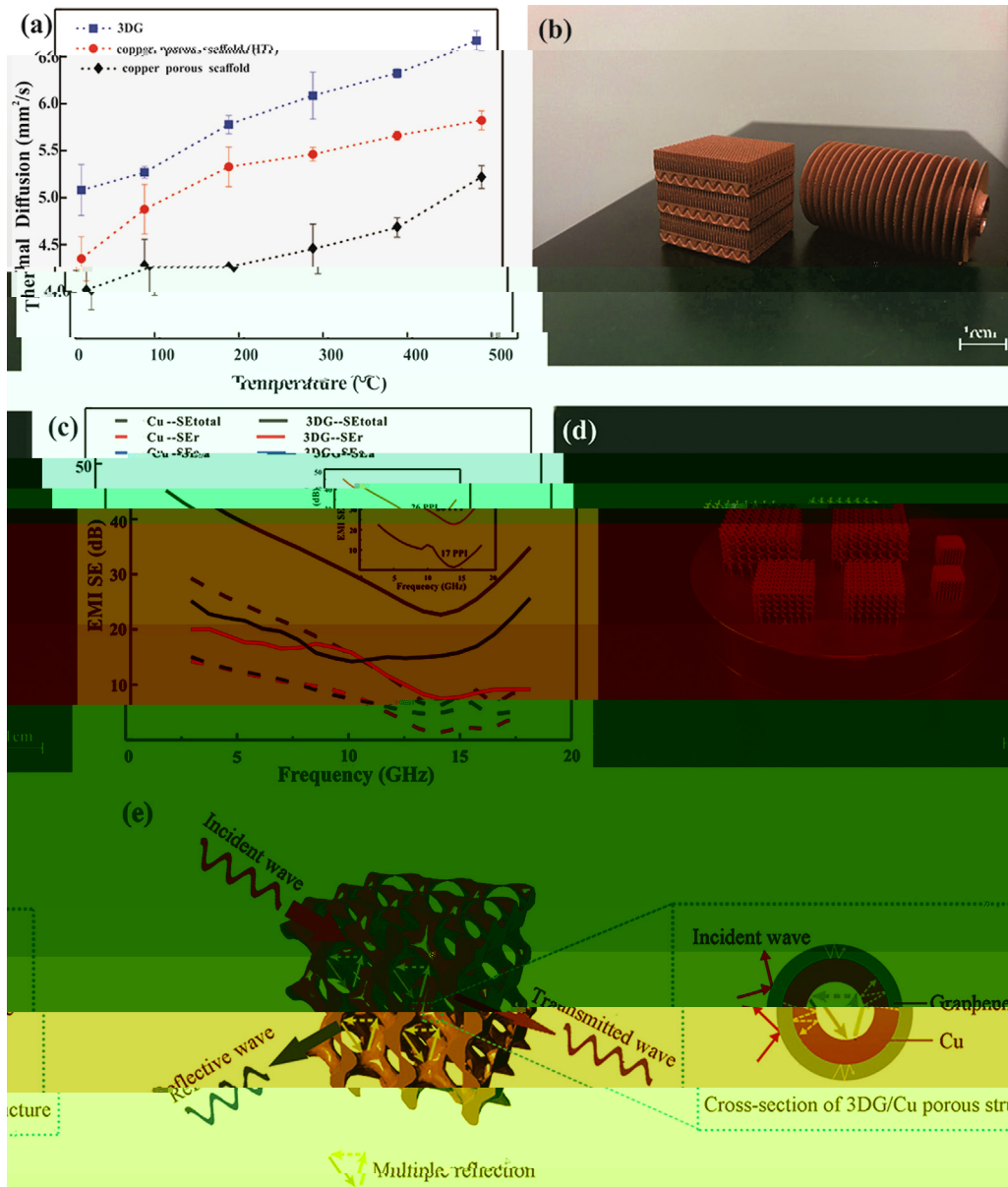


Fig. 9. Performance of 3DG/C porous scaffold: (a) Thermal Diffusion; (b) SLM porous scaffold structure; (c) EMI SE; (d) Cross-section of porous scaffold; (e) Schematic of 3DG/C porous scaffold EMI. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

Table 1

Comparison of the maximum shielding efficiency and improvement of thermal property of various porous structures.

Coating materials	Substrate	Method	Maximum shielding efficiency (dB)	Improvement of thermal property (%)	Ref
G	Al	Infiltration + sintering + CVD	37	-	50]
G	PS	Hierarchical porous structure	29.3	-	56]
G	PMMA	Sintering + infiltration + CVD	19	-	57]
C /G	/C	Sintering + infiltration + CVD	-	8.5	58]
G	Ni	Fabrication + CVD	-	554	59]
G	C-Ni	Electroless plating + infiltration + sintering	20	-	60]
G	C	Precipitation + CVD	-	2.4	61]
G	Al	Fabrication + infiltration	47	6.3	62]
G	C	CVD + SLM	47.8	27	This work

Note: Poly (ethylene terephthalate)-PPMA, polystyrene-PS.

test HT results suggest that the *in-situ* effect (Fig. 9a). Significant differences were observed between the 3DG/C composite and HT results. It is observed that the HT results show a significant increase in the number of pores (1–2 μm) compared to the *in-situ* results. This is due to the fact that the *in-situ* process is more uniform and stable. With the use of SLM, the pore size distribution (Fig. 9b) is significantly different from the HT results. The *in-situ* process shows a higher density of pores, which is beneficial for the mechanical properties of the composite. The results of the tensile test (Table 1) show that the *in-situ* process results in a higher tensile strength compared to the HT process. This is due to the fact that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite.

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SEM analysis shows that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite. The results of the tensile test (Table 1) show that the *in-situ* process results in a higher tensile strength compared to the HT process. This is due to the fact that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite. The results of the tensile test (Table 1) show that the *in-situ* process results in a higher tensile strength compared to the HT process. This is due to the fact that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite.

4. Conclusions

At the 3DG/C composite, the *in-situ* process results in a higher tensile strength compared to the HT process. This is due to the fact that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite. The results of the tensile test (Table 1) show that the *in-situ* process results in a higher tensile strength compared to the HT process. This is due to the fact that the *in-situ* process results in a more uniform and stable structure, which is beneficial for the mechanical properties of the composite.

Credit authorship contribution statement

Kaka Cheng: Conceptualization, Methodology, Formal analysis, Writing - original draft. Wei Xiong: Visualization, Writing - original draft. Yan Li: Writing - original draft, Funding acquisition. Rongsheng, Shaojie. Liang Hao: Formal analysis. Chunze Yan: Resources, Formal analysis. Zhaoqing Li: Visualization. Zhufeng Liu: Formal analysis. Yushen Wang: Investigation, Software. Khamis Essa: Writing - original draft. Li Lee: Data curation. Xin Gong: Software. Ton Peijs: Writing - original draft, Supervision.

Declaration of Competing Interest

The authors declare that they have no competing interest.

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Appendix A. Supplementary data

Supplementary data to this article is available at <https://doi.org/10.1016/j.jes.2020.105904>.

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